SECTION D

VARIABLE LOAD SPRING SUPPORTS

VARIABLE LOAD SPRINGS

SPRING SWAY BRACES (APV)

SMALL SPRINGS

SPRING ANTI-VIBRATING CLAMPS

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



CONTENTS

- VARIABLE LOAD SPRINGS	D-1
- LOAD TABLE	D-2
- GENERAL DIMENSIONS FOR VARIABLE LOAD SPRING SUPPORTS	D-3
- GENERAL ASSEMBLY CONSIDERATIONS	D-7
- SPECIAL CORROSION RESISTANT SUPPORTS AND CONTINUOUS BLOCKING SYSTEM	D-22
- CONTINUOUS BLOCKING SYSTEM	D-23
- RECOMMENDATIONS FOR OPERATION AND MAINTENANCE ON SITE.	D-27
- SPRING SWAY BRACES (APV)	D-28
- SMALL SPRING	D-29
- SPRING ANTI-VIBRATION CLAMP	D-30
- DOUBLE SPRING ANTI-VIBRATION CLAMP	D-31

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



VARIABLE LOAD SPRING SUPPORTS

Variable load spring supports are installed in a piping system when relatively small (up to 80 mm) vertical movements need to be absorbed. They are generally related to thermal expansions or contractions. The springs always work under compression.

They are made up of a helical spring, inserted into a cylindrical housing with a welded or bolted down construction. Riveted to the support is a scaleplate indicating the model, type, size, loads and movement.

Springs are classified according to the MODEL-SIZE-TYPE combination.

MODEL

There are four models: CVC, CV, CVL and CVLL. They support the same loads, but they are differentiated by the vertical travels that they accept.

In order to select the suitable model, it should be taken into account that the variation in load from the cold position of the spring to the hot position must be equal to or less than 25%. This value is accepted by the majority of the national and international standards, but however, it is the project engineer who should set this variability or an even lower threshold, conducting an individualized study for each specific case.

According to this latter criterion, the result is approximately as follows:

- MODEL CVC \rightarrow $\Delta y \leq 12 \text{ mm.}$
- MODEL CV \rightarrow 12 mm < $\Delta y \le 25$ mm.
- MODEL CVL \rightarrow 25 mm < $\Delta y \le$ 50 mm.
- MODEL CVLL \rightarrow 50 mm < $\Delta y \le 80$ mm.

Where Δy is vertical movement.

Where ABS (CL - HL) is the absolute value resulting from deducting the cold load (CL) from the hot load (HL).

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



SIZE

Spring size is indicated by a number, from 1 to 21, and determines the load range that the spring can support. This is selected using the loads table and in terms of the characteristics of the variable load supports (page 19). In this table, there are two zones (upper and lower) indicated as "safety margins". These zones should never be considered as operating positions. The selection criterion is as follows: depending on the specified operating load (also known as "hot load"), a load is chosen from the table, either equal to or greater than the required load. It is recommended to select a load in the central zone of the table, so that the operating position of the spring is as centred as possible on the total travel of the spring (life span will be greater and there will be more margin for readjusting the load or for absorbing variations in the design). It can be noted that, depending on the model of the spring, the total travel varies, the CVLL model being the one that accepts a longer travel, as indicated in the section MODEL. This is related to the spring rate (kg/mm), a value indicated below the size of the spring. The greater the movements, the lower the value of the spring rate.



				27
21/07/10	GENERAL REVISION	DDG	EAR	
DATE	EDITED FOR :	DRAW.	REV.	

0

REV



																															_					
			21		250	125	62,5	41,67		3750	4375	5000	5625	6250	6875	7500	8125	8750	9375	0000	0625	1250	1875	2500	3125	3750	4375	5000	5625	6250	6875	7500	21		M-64	
	S		20	1	170	85	42,5	28,33 4		3400	3825	4250	4675	5100	5525	2950	6375	6800	7225	7650 1	8075 1	8500 1	8925 1	9350 1	9775 1	0200	0620	1050	14701	1900	2325 1	2750 1	20		M-56	
	POR		19		125	62,5	31,25	20,83		2500	2812 :	3125	3437	3750	4062	4375	4687 (5000	5312	5625	5937	3250	3562	3875	7187	7500 1	7812 1	3125 1	3437 1	3750 1	9062 1	9375 1	19		N-48	
	s SUP		18	1	94	47	23,5	15,67		1880	2115	2350	2585	2820	3055 .	3290	3525	3760	3995	4230	4465	4700	4935 (5170	5405	5640	5875	6110	6345	6580	6815	7050	18		M-42	
	RING		17	1	70	35	17,5	11,67		1400	1575	1750	1925	2100	2275	2450	2625	2800	2975	3150	3325	3500	3675	3850	4025	4200	4375	4550	4725	4900	5075	5250	17		36	
	AD SF		16		52	26	13	8,667		1040	1170	1300	1430	1560	1690	1820	1950	2080	2210	2340	2470	2600	2730	2860	2990	3120	3250	3380	3510	3640	3770	3900	16		Ň	
	Е ГО/		15	1	39	19,5	9,75	6,5		780	878	975	1072	1170	1267	1365	1462	1560	1657	1755	1852	1950	2047	2145	2242	2340	2437	2535	2632	2730	2827	2925	15		30	
	IABL		14		29	14,5	7,25	4,833		580	652	725	797	870	942	1015	1087	1160	1232	1305	1377	1450	1522	1595	1667	1740	1812	1885	1957	2030	2102	2175	14		М-	
I	: VAR		13		22	1	5,5	3,667		440	495	550	605	660	715	770	825	880	935	066	1045	1100	1155	1210	1265	1320	1375	1430	1485	1540	1595	1650	13	Kg.	24	
I	F THE	Щ	12	d/mm	16,5	8,25	4,125	2,75	ie 20.	330	371	413	454	495	536	578	619	660	701	742	784	825	866	908	949	990	1030	1070	1113	1155	1196	1237	12	DS IN	Þ	
	cs ol	RT SIZ	11		12,5	6,25	3,125	2,083	vpe will t	250	281	313	344	375	406	438	469	500	531	562	593	625	656	687	719	750	781	813	844	875	906	938	11	- LOA	-20	
	RISTI	UPPO	10	IG RA	9,5	4,75	2,375	1,583	for a G-tj	190	214	238	261	285	309	333	356	380	404	428	451	475	499	523	547	570	594	618	641	665	689	713	10	t size	ž	
	ACTEI	S	6	SPRIN	7,25	3,625	1,813	1,208	nun size	145	163	181	200	218	236	254	272	290	308	326	345	363	381	399	417	435	453	471	490	508	526	544	6	PPOR		
	HAR/		8		5,5	2,75	1,375	0,917	e maxim	110	124	138	151	165	179	193	206	220	234	248	261	275	289	303	316	330	344	358	371	385	399	413	8	SU	M-16	
	ND C		2		4	7	-	0,667	one. Th	80	60	100	110	120	130	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	7			
	ILE A		9		с	1,5	0,75	0,5	to each	60	68	75	83	60	98	105	113	120	128	135	143	150	158	165	173	180	188	195	203	210	218	225	9			
	O TAE		5		2,3	5 1,15	3 0,575	2 0,383	esponds	46	52	58	63	69	75	81	86	92	98	103	109	115	121	127	132	138	144	150	155	161	167	173	5			
	LOAE		4		1,75	5 0,875	3 0,438	3 0,292	elow corr	35	39	44	48	53	57	61	66	70	74	79	83	88	92	96	100	105	109	114	118	123	127	131	4		1-12	
	TING		3		1,25	0,62!	0,313	7 0,208	hown b€	25	28	31	34	38	4	44	47	50	53	56	59	62	99	69	72	75	78	81	84	88	91	94	3		2	
	ERA.		2		1	5 0,5	8 0,25	5 0,16	on data s	20	23	25	28	30	33	35	38	40	43	45	48	50	53	55	58	60	63	65	68	20	73	75	2			
	Ğ		-		0,75	0,37	0,18	L 0,12	nformatic	15	17	19	21	23	24	26	28	30	32	34	36	38	39	41	43	45	47	49	51	53	54	56	٢		Ļ	
																			-		_										_	/١				
	- CVL								NIDY	0	15	30	45	60	75	90	105	120	135	150	165	180	195	210	225	240	255	270		<u> </u>	- CVL		ш			
	CVI	с то с ш ц то с то развити с то с то с то с то с то с то G-type is							T IVIA	0	10	20	30	40	50	60	20	80	90	100	110	120	130	140	150	160	170	180			CVI	ODEL	D SIZ			
	C C									0	5 5	10	5 15	20	5 25	30	5 35	40	5 45	50	5 55	60	5 65	70	5 75	80	5 85	06		- U L A	c CV	ž	RC			
	Č	4	Ξ		о п 	」 IL	Ö.	Т	ease, No	Ŭ	õ	0	2,5	5	7,5	10	12 12	15	11 12	20 50	22, 72,	ц 25	0 27,	а А а Ю	3, 3, 70	35	37,	40	42,	45	Ŭ	ñ	Š			
	MOD	ອ	NIC	סאנ	DAS	SES	Ю	o	* Pl									٩D	A -	IΞΛ	АЯ	Γ٦	AT	οι	-											
	21/07/10			G	ENE	ERA		REV	ISIC	DN				DG		EA	2										(1								
	12/07/91 17/01/85				IN IN	FOI FOI	RM/	ATIC ATIC	лс ЛС				J	MD IRS	╉	EAI EAI	≺ २											-		-			5	Y	2	
	DATE	EDITED FOR :							DF	RAV	v.	RE\	/.					1		5			p	ipe	e h	an	106	er	50	lu	tio	n:				

REV

VARIABLE LOAD SPRING SUPPORTS

SECTION D 3

	VA	R		4	B	L	.E		L	.0)/	4	D	S	SF	PF	R	N	IC)	S	U	P	P	۲ C)F	۲	Γ	5				SE	EC 3	ТI -Е	IO BIS	N D
			21		2452	1226	212.0	0 1 Z, Y	408,7		36,78	42,91	49,04	55,16	61,29	67,42	73,55	79,68	85,81	91,94	98,07	104,2	110,3	116,5	122,6	128,7	134,9	141,0	147,1	153,2	159,4	165,5	171,6	21		M-64	
	6		20		1667	833.6	110.00	4 10,0	2///8		33,34	37,51	41,68	45,85	50,02	54,18	58,35	62,52	69'99	70,86	75,02	79,19	83,36	87,53	91,70	95,86	100,0	104,2	108,4	112,5	116,7	120,9	125,0	20		M-56	
	ORTS		19		1226	613.0	2,0,0		204,3		24,52	27,58	30,65	33,71	36,78	39,84	42,91	45,97	49,04	52,09	55,16	58,22	51,29	34,35	37,42	70,48	73,55	76,61	79,68	32,74	35,81	38,87	91,94	19		M-48	
	SUPF		18		921,9	461.0	2 0 0 0	C, U, D	153,7		18,44 2	20,74	23,05 (25,35	27,66	29,96	32,27	34,57	36,87	39,18 {	41,48	43,79 !	46,09 (48,40 (50,70 (53,01	55,31	57,62	59,92	62,23	64,53	66,83	69,14 (18		M-42	
	RING		17		386,5	343.3	174.6	0, 1	114,5		13,73	15,45	17,16	18,88	20,59	22,31	24,03	25,74	27,46	29,18	30,89	32,61	34,32	36,04	37,76	39,47	41,19	42,91	44,62	46,34	48,05	49,77	51,49	17		6	
	AD SP		16		510,0 (255.0	107 1	0, 121	85,01		10,20	11,47	12,75	14,02	15,30	16,57	17,85	19,12	20,40	21,67	22,95	24,22	25,50	26,77	28,05	29,32	30,60	31,87	33,15	34,42	35,70	36,97	38,25	16		M-3	
	E LOA		15		382,5 {	101 2	2, 10	10,02	53,75		7,65	8,61	9,56	10,51	11,47	12,43	13,39	14,34	15,30	16,25	17,21	18,16	19,12	20,07	21,04	21,99	22,95	23,90	24,86	25,81	26,77	27,72	28,69	15		0	
	IABLI		14		284,4	142 2	71 10	1,10	47,40 0		5,69	6,39	7,11	7,82	8,53	9,24	9,95	10,66	11,38	12,08	12,80	13,50	14,22	14,93	15,64	16,35	17,06	17,77	18,49	19,19	19,91	20,61	21,33	14		M-3	
	E VAR		13		215,8	107 0		00,04	35,96		4,32	4,85	5,39	5,93	6,47	7,01	7,55	8,09	8,63	9,17	9,71	10,25	10,79	11,33	11,87	12,41	12,95	13,48	14,02	14,56	15,10	15,64	16,18	13	kN.	4	
	F THE	ZE	12	N/mm	161,8	80 91	10,00	40,40	26,97	3 is 20.	3,24	3,64	4,05	4,45	4,85	5,26	5,67	6,07	6,47	6,87	7,28	7,69	8,09	8,49	8,90	9,31	9,71	10,10	10,49	10,92	11,33	11,73	12,13	12	NI SOV	M-2	
	ICS O	ORT SI	11	ATE IN	122,6	61.29	20.65	20,00	20,43	a Type (2,45	2,76	3,07	3,37	3,68	3,98	4,30	4,60	4,90	5,21	5,51	5,82	6,13	6,43	6,74	7,05	7,36	7,66	7,97	8,28	8,58	8,89	9,20	11	E - LO/	0	
	ERIST	SUPP(10	R R	93,17	46.58	22,20	40,0U	15,52	ו size for	1,86	2,10	2,33	2,56	2,79	3,03	3,27	3,49	3,73	3,96	4,20	4,42	4,66	4,89	5,13	5,36	5,59	5,83	6,06	6,29	6,52	6,76	6,99	10	RT SIZ	M-2	
	RACTE		6	SPR	71,10	35 55	17 70	11,10	11,85	maximur	1,42	1,60	1,78	1,96	2,14	2,31	2,49	2,67	2,84	3,02	3,20	3,38	3,56	3,74	3,91	4,09	4,27	4,44	4,62	4,81	4,98	5,16	5,34	6	IDPPOI		
	CHAF		8		53,94	26.97	10,01	10,40	8,99	half. The	1,08	1,22	1,35	1,48	1,62	1,76	1,89	2,02	2,16	2,29	2,43	2,56	2,70	2,83	2,97	3,10	3,24	3,37	3,51	3,64	3,78	3,91	4,05	8	S	M-16	
	AND		2		39,23	19.61	200	0,0 1	6,54	to each I	0,78	0,88	0,98	1,08	1,18	1,27	1,37	1,47	1,57	1,67	1,77	1,86	1,96	2,06	2,16	2,26	2,35	2,45	2,55	2,65	2,75	2,84	2,94	7			
	ABLE		9		3 29,42	3 14 71	200 2	, v v, v	4,90	esponds	0,59	0,67	0,74	0,81	0,88	0,96	1,03	. 1,11	1,18	1,26	1,32	1,40	1,47	1,55	1,62	1,70	1,77	1,84	1,91	1,99	2,06	2,14	2,21	9			
	AD T		5		6 22,5(11 25	, , , , , , , , , , , , , , , , , , ,	0,04	5 3,76	elow corr	4 0,45	3 0,51	3 0,57	7 0,62	2 0,68	3 0,74	0,79	5 0,84	9 0,90	3 0,96	7 1,01	1 1,07	5 1,13	0 1,19	4 1,25	3 1,29	3 1,36	7 1,41	2 1,47	3 1,52	1 1,58	5 1,64	3 1,70	5			
	IG LO		4		26 17,1	3 8 55	2,0		4 2,80	shown be	5 0,32	7 0,38	0 0,4;	3 0,4	7 0,52	0 0,5(3 0,6(6 0,6!	9 0,6	2 0,7:	5 0,7	8,0,8	1 0,8(5 0,9(8 0,9	1 0,98	4 1,00	6 1,07	9 1,12	2 1,16	6 1,2	9 1,2!	2 1,28	4		M-12	
	RATIN		3		31 12,2	6 1		D'0 0	04 Z,U	the data	20 0,2	23 0,2	25 0,3	27 0,3	29 0,3	32 0,4	34 0,4	37 0,4	39 0,4	t2 0,5	t4 0,5	47 0,5	49 0,6	52 0,6	54 0,6	57 0,7	59 0,7	32 0,7	34 0,7	37 0,8	39 0,8	72 0,8	74 0,9	3			
	OPE	1 2 36 9,81 68 4,90 68 2,45 23 1,64 23 1,64 unit and th 1 15 0,20 17 0,23						19 0,2	21 0,2	23 0,2	24 0,3	25 0,3	27 0,3	29 0,3	31 0,4	33 0,4	35 0,4	37 0,4	38 0,5	40 0,5	42 0,5	44 0,5	46 0,6	48 0,6	50 0,6	52 0,6	53 0,7	55 0,7	1 2								
	ОЕГ	MOI 0, 11, 12, 12, 12, 12, 14, 14, 14, 14, 14, 14, 14, 14, 14, 14						,	Ő	Ó	Ó	Ó	Ó	Ó	o	Ó	Ó	Ó	Ó	, O	Ó	Ó	Ó	Ó	Ó	Ó	ó	Ó			Λ						
	, CLL	◄	ш	с I	lo o i	Ш.	<u>ן</u> ר (ناد دوځ	່ <u>ບ</u> -	s a doub		Z C	0	15	30	45	60	75	06	105	120	135	150	165	180	195	210	225	240	255	270		2 C	ארר		ĺ	
	CVL C	A	ш	с I	<u>م</u>	ш	т (ב פ	5	Type G i		MAR	0	10	20	30	40	50	60	20	80	06	100	110	120	130	140	150	160	170	180		MAR	CVL C	DEL	d Size	
	c	A	ш	с I	ום	ш	тÇ	ב פ	5	that the			0	5	10	15	20	25	30	35	40	45	50	55	60	65	70	75	80	85	60			C۷	M	RO	
	cvc	A	ш	U I	ום	ш	т (בפ	=	ase note		る	0	2,5	5	7,5	10	12,5	15	17,5	20	22,5	25	27,5	30	32,5	35	37,5	40	42,5	45	5	ה	cvc			
	MOD.	ອ	NIC	E INC	191 293	SE SE	ิย	00	,	* Ple								ΤS	ool AD	IA . 19U	I S NEI	/A/ I)/	/3 = ר בי	АТ 10	OT QAD	г											
3	21/07/10			G	EN	ER	AL	RE	EVI	SIC	DN				DC	;	EA	R	_									(1								
2	12/07/91 17/01/85				יו וו			MA. MA.		N N				• .	JMD JRS	+	EA	R R				(1		-			5	Y	2	
REV.	DATE	EDITED FOR :							D	RAV	v.	RE\	<i>.</i>							5			р	ipe	e ł	Iai	nge	er	50	lui	tion	ns					



welding lug

rod

double welding lug

rod

TYPE C

TYPE E

Welded to

structure - hanging

TYPE

The different types of support are classified by a letter - from A to H - and are differentiated by the assembly conditions regarding connection to the structure.

TYPE B







Support on structure - hanging

TYPE F



Support on







0	21/07/10	GENERAL REVISION	DDG	EAR	
REV.	DATE	EDITED FOR :	DRAW.	REV.	pipe hanger solutions

ORDER

To place an order, the following details must be indicated:

- Model, size and type.
- Hot and/or cold load.
- Vertical movement ("travel") of the pipe from the cold position to the hot position. If movement is upwards, indicate so with the positive sign (+), and with the sign (-) if movement is downwards.
- Identification mark ("tag number").
- Options: corrosion resistant / continuous blocking.

Note that on a variable load spring, the following condition is always met:

$\mathbf{CL} = \mathbf{HL} + \Delta \mathbf{y} \cdot \mathbf{k}$

Where "k" is the spring rate (depending on the model selected). For this reason, different combinations of cold load, hot load and movement are given for each spring manufacturer.

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



TRAVEL STOPS

Unless required otherwise, the support will be preset on the cold or installation load, by two travel stops. These stops should not be removed until the installation stages and hydraulic testing are completed. Once removed (with the plant still "cold"), the indicator should coincide with the peak of the cold load / installation load indicator. When the plant starts up, the indicator will tend to shift until it coincides with the position of the hot load / operating load indicator.

The operating position for the spring is theoretical, i.e., it is designed for "ideal" work conditions; in real life conditions, certain factors can come into play that affect the actual operationg position of the spring. For instance, a spring located on a draining line will normally be in the cold position, and will only move when draining really causes change of load and temperature on the piping.







0	21/07/10	GENERAL REVISON	DDG	EAR	
REV.	DATE	EDITED FOR :	DRAW.	REV.	



GENERAL INSTALLATION AND OPERATION CONSIDERATIONS:

In this section, we set out to indicate the general aspects to be considered in order to carry out a correct installation of the variable load spring supports, as well as explaining precautions to take for correct working order and subsequent maintenance of said elements.

Firstly, in order to avoid the thermal movements of the piping being restrained, it should be taken into account that the installed accessories may cause interference with other elements that have nothing to do with supporting the piping.

This possibility often occurs when the supports are fitted with rods of a certain length, since throughout their length, they may approach the beams, other piping or accessories which, due to their proximity, may cause said interference.

To make identification of the supports easy, it is advisable to position the spring support in such a manner that the scaleplate is on the side with the best visibility.

When welding to install the support, they must be coated with the appropriate paint in order to avoid any oxidation that may spread to the housing, leading to undesirable damage.

It is appropriate that, in the threaded zones, grease is applied in order to avoid deterioration due to oxidation, that may make subsequent adjustment or dismantling operations difficult.

We recommend that once the spring support is finally installed, the travel stops should be kept so that they can be used in the event of having to dismount the support for inspection, recalibrating, etc., or to carry out changes of piping accessories. However, if not available, temporary blocking may be achieved with plates and profiles that may be tack welded to the spring casing.

Since during plant maintenance operations, touching up paintwork of the supporting elements is part of these activities, special care should be taken not to paint the sliding surfaces, threaded zones and scaleplates.

As a final recommendation, it should be remembered that it is appropriate to conduct a visual inspection of all the spring supports installed on the pipeline before starting up, in order to ensure that all the travel stops have been removed, that the springs are correctly positioned and that all the lock nuts are tightened.

IDENTIFICATION CARD MODEL CVC



2	21/07/10	GENERAL REVISION	DDG	EAR
1	20/10/98	INFORMATION	JMD	EAR
0	04/09/94	INFORMATION	BM	JMD
REV.	DATE	EDITED FOR :	DRAW.	REV.



INSTALLATION INSTRUCTIONS FOR VARIABLE LOAD SPRING SUPPORTS

Before installing a variable load support, there must be a provisional, rigid support able to sustain the piping in its correct position so that no deformities occur on the same nor overstresses occur at any of its points.

Once the point has been located where the variable load support should be fitted, install all the accessories, both on the piping and on the supporting structure, according to the design drawings for the support.

Depending on the type of spring support selected, certain manoeuvres will have to be carried out, until the supporting element can take the required load.

INSTALLATION INSTRUCTIONS



SPRINGS TYPE A, B and C.

For these types of springs, once the relevant accessories have been installed (clamp, lug, rods, eye nuts, beam attachments, etc.), locate them in the position of COLD PRESET LOAD. To do so, act on the adjustment turnbuckles until the travel stops are loose and can be removed by hand or, at the most, with the help of pliers.

The operation of removing the travel stops must be carried out once the hydraulic test is completed, and on the condition that no other manoeuvres are going to be carried out on the piping that may leave the spring out of its position in COLD PRESET LOAD.

When the piping reaches the temperature considered in the stress analysis, the spring position indicator should indicate OPERATING LOAD, which will be located above or below that of COLD PRESET LOAD, depending on the vertical displacement at that point.

1	21/07/10	GENERAL REVISION	DDG	EAR
0	04/09/94	INFORMATION	BM	JMD
REV.	DATE	EDITED FOR :	DRAW.	REV.



INSTALLATION INSTRUCTIONS

TYPE D SPRINGS

To install this type of spring, once the corresponding accessories have been fitted (clamp, lug, rods, etc.), some welding may have to be carried out to join the spring housing to the supporting structure in order to ensure the position of the element in terms of any incident caused by manoeuvres close to the supporting point, or any transitional vibration in the piping.



In order to ensure that the spring takes the COLD PRESET LOAD, act on the nut located in the upper part of the rod, until the travel stops can be released by hand or, at the most, with the help of a hand tool such as pliers.

The operation of removing the travel stops must be carried out once the hydraulic test is completed, and on the condition that no other manoeuvres are going to be carried out on the piping that may leave the spring out of its position in COLD PRESET LOAD.

When the piping reaches the temperature considered in the stress analysis, the spring position indicator should indicate OPERATING LOAD, which will be located above or below that of COLD PRESET LOAD, depending on the vertical displacement at that point.

1	21/07/10	GENERAL REVISION	DDG	EAR
0	04/09/94	INFORMATION	BM	JMD
REV.	DATE	EDITED FOR :	DRAW.	REV.



INSTALLATION INSTRUCTIONS

SPRINGS TYPE E

As in the case of Type D springs, to install this type of spring, once the corresponding accessories have been fitted (clamp, lug, rods, etc.), some welding may have to be carried out to join the spring housing to the supporting structure in order to ensure the position of the element in terms of any incident caused by manoeuvres close to the supporting point, or any transitional vibration in the piping.



INSTALLATION INSTRUCTIONS

SPRINGS TYPE F

Installation of this type of spring on the supporting structure is made by means of bolts located in the holes in the base plate, although if the structural arrangement does not allow for this, or if it is preferred, said spring base plate can also be welded to the supporting structure, in order to ensure that the unit does not turn over or move from its position in the case of movements, in the horizontal plane, of the pipe.





To ensure that the spring takes the COLD PRESET LOAD, act on the threaded load column located in the upper part of the housing, until the travel stops can be released by hand or, at the most, with the help of a hand tool such as pliers.

The operation of removing the travel stops must be carried out once the hydraulic test is completed, and on the condition that no other manoeuvres are going to be carried out on the piping that may leave the spring out of its position in COLD PRESET LOAD.

When the piping reaches the temperature considered in the stress analysis, the spring position indicator should indicate OPERATING LOAD, which will be located above or below that of COLD PRESET LOAD, depending on the vertical displacement at that point.

1	21/07/10	GENERAL REVISION	DDG	EAR
0	04/09/94	INFORMATION	BM	JMD
REV.	DATE	EDITED FOR :	DRAW.	REV.



INSTALLATION INSTRUCTIONS

SPRINGS TYPE G



For these types of springs, once the relevant accessories have been installed (clamp, lug, rods, eye nut, beam attachment, etc.), locate them in the position of COLD PRESET LOAD.

To ensure that the springs take the COLD PRESET LOAD, act on the adjustment turnbuckles until the travel stops are loose and can be removed by hand or, at the most, with the help of pliers. It is advisable that the adjustment operation is carried out alternating between the two springs, or simultaneously on both, if possible.

The operation of removing the travel stops must be carried out once the hydraulic test is completed, and on the condition that no other manoeuvres are going to be carried out on the piping that may leave the spring out of its position in COLD PRESET LOAD.

When the piping reaches the temperature considered in the stress analysis, the spring position indicator should indicate OPERATING LOAD, which will be located above or below that of COLD PRESET LOAD, depending on the vertical displacement at that point.

It is advisable to apply some welding points to join the pipe shoe (if there is one) to the center of the beams which connect the springs, if the movements occurring in the horizontal plane justify it. In this way, it will avoid the piping displacement towards one of the springs and thus ensure that both are subject to the same load.

1	21/07/10	GENERAL REVISION	DDG	EAR
0	04/09/94	INFORMATION	BM	JMD
REV.	DATE	EDITED FOR :	DRAW.	REV.



INSTALLATION INSTRUCTIONS

SPRINGS TYPE H

TYPE H



As in the case of Type F springs, the installation of this type of spring is by means of welding the lower element, the rear bracket, to the support structure. At the upper end, a clamp can be installed (Option 1) or another rear bracket (Option 2).

In order to ensure that the spring reaches the COLD PRESET LOAD, it is essential to act on the upper threaded load column until the travel stops can be released by hand, or at the most, with the help of a hand tool such as pliers.

The operation of removing the travel stops must be carried out once the hydraulic test is completed, and on the condition that no other manoeuvres are going to be carried out on the piping that may leave the spring out of its position in COLD PRESET LOAD.

When the piping reaches the temperature considered in the stress analysis, the spring position indicator should indicate OPERATING LOAD, which will be located above or below that of COLD PRESET LOAD, depending on the vertical displacement at that point.

1	21/07/10	GENERAL REVISION	DDG	EAR
0	04/09/94	INFORMATION	BM	JMD
REV.	DATE	EDITED FOR :	DRAW.	REV.



VARIABLE LOAD SPRING SUPPORT SECTION D										
TYPE A 14										14
				SIZE	MOD.	ØA	C*	D*	ØR	WEIGHT (Kg.)
				1	CVC CV	08	45 10	177 236	M12v1 75	3,5 5
				1	CVL CVLL	90	10 10	401 588		7 8,5
			F	-	CVC CV		45 10	177 241		3,5 5
				2	CVL	98	10	415	M12x1,75	7 85
			F		CVC		45	182		3,5
				3	CVL	98	10	435	M12x1,75	7,5
			ŀ		CVLL		45	182		9,5
				4	CV CVL	98	10 10	246 439	M12x1,75	5 7,5
			ŀ		CVLL CVC		10 45	645 187		9,5 4
		I		5	CV CVL	98	10 10	251 451	M12x1,75	5 7,5
		ØR	ŀ		CVLL		10 50	663 204		9,5 7
				6	CV CV	134	15	268 485	M12x1,75	9 14
					CVLL		15	696		14
				7	CVC CV	134	15	209	M16x2	10
	4				CVL		15 15	508 738		15 19
				8	CVC CV	134	50 15	214 298	M16x2	7,5 11
				0	CVL CVLL	104	15 15	543 788	INTOX2	17 22
			ſ		CVC CV	10.1	50 25	230 330		8 11
				9	CVL CVL	134	25 25	595 850	M16x2	18 23
			Ē		CVC CV		55	245 340		8
		P 00104A C 24200 C 25200 C 251000 WARCA (TAG		10	CVL	134	25	605	M20x2,5	19
	D		F				55	247		18
				11	CVL	168	25	622	M20x2,5	23 35
			ŀ		CVLL		25 55	902 257		44 19
				12	CV CVL	168	25 25	357 652	M24x3	25 38
			ŀ		CVLL CVC		25 50	947 282		49 21
				13	CV CVL	168	25 25	377 680	M24x3	27 43
			ŀ		CVLL CVC		25 70	987 312		57 23
	<u> </u>			14	CV CVL	168	30 30	415 750	M30x3,5	30 50
			ŀ		CVLL		<u>30</u> 80	1085 325		68 46
				15	CV CV	236	30	415 750	M30x3,5	59 80
			ļ		CVLL		30	1085		113
				16	CVC CV	236	40	450	M36x4	67
			Ļ				40	1170		139
				17	CVC	236	80 40	350 510	M36x4	59 79
					CVL CVLL	200	40 40	900 1290		130 172
<u>N.B</u>	<u>.:</u>			18	CVC CV	30/	60 40	370 510	M42x4 5	106 134
* (C and D an	e approximate dimensions which		10	CVL CVLL	504	40 40	900 <u>129</u> 0		204 264
c	orrespond	to the vertical position at the lowes	t 「	10	CVC CV	20.4	60 40	380 525	M40F	120 152
	bad value o	of the working range. Therefore, the	•	19	CVL CVLL	304	40 40	955 1385	11/148X5	243 323
a Io	bad applied	holono will vary depending on the	f		CVC CV		60 40	390 550		138 176
				20	CVL	304	40	1005	M56x5,5	291 300
			ŀ				60	420		160
				21	CVL	304	70	1240	M64x6	373
3	21/07/10	GENERAL REVISION	DDG	EAR		I	<u> </u> /U	1/90	1	520
2	12/07/91	INFORMATION	JMD	EAR						
1	17/01/85	INFORMATION	JRS	EAR						
REV.	DATE	EDITED FOR :	DRAW	. REV.			p	ipe ho	inger s	olutions
-							195	~~	8-C7	





VARIABLE LOAD SPRING SUPPORT TYPE D

SIZE

MOD.

ØA

G*

ØR

SECTION D 17

WEIGHT (Kg.)



1	CV CV	98	355 630	M12x1,75	5
			927 205		8,5 3,5
2	CV CVL	98	360 645	M12x1,75	5 7
	CVLL CVC		948 210		8,5 3,5
3	CV CVL	98	365 665	M12x1,75	5 7,5
	CVLL CVC		210		4
4	CVL CVLL	98	670 984	M12x1,75	7,5 9,5
5	CVC CV	98	215 370	M12x1.75	4
			680 1002		7,5 9,5 7
6	CV CVL	134	380 700	M12x1,75	9 14
	CVLL CVC		1028 230		18 7
7	CV CVL	134	390 730	M16x2	10 15
			240		7,5
8	CVL CVLL	134	765	M16x2	17
٩	CVC CV	134	250 420	M16x2	8 11
3	CVL CVLL	134	790 1160	WITUXZ	18 23
10	CVC CV	134	255 430 805	M20x2,5	12 19
	CVLL CVC		1180 280		24 18
11	CV CVL	168	460 850	M20x2,5	23 35
			1240 290 475		45
12		168	880 1285	M24x3	38
13	CVC CV	168	295 490	M24x3	21 27
			905 1320 315		43 50 23
14	CV CVL	168	520 975	M30x3,5	30 50
	CVLL CVC		1430 325		55 46
15	CV CVL	236	520 960	M30x3,5	59 89
10	CVC CV	000	340 550	M004	52 67
10	CVL CVLL	230	1020 1490	1013024	106 138
17	CVC CV	236	365 595 1115	M36x4	59 79 130
			1625 385		172 106
18	CV CVL	304	600 1095	M42x4,5	134 204
			1585 415		262 120
19	CVL CVL	304	1185 1720	M48x5	243 323
20	CVC CV	304	430 670	M56x5.5	138 176
20	CVL CVLL	504	1235 1790		291 390
21	CVC CV	304	455 770 1440	M64x6	219 373
<u>, </u>	CVLL		2110		520
-					

pipe hanger solutions

<u>N.B.:</u>

* G is an approximate dimension which corresponds to the vertical position at the lowest load value of the working range. Therefore, the actual dimension will vary depending on the load applied.

3	21/07/10	GENERAL REVISION	DDG	EAR
2	12/07/91	INFORMATION	JMD	EAR
1	17/01/85	INFORMATION	JRS	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



SECTION D 18



		~.			
SIZE	MOD.	ØA	В	ØR	WEIGHT (Kg.)
	CVC		145		3,5
1		98	240	M12x1,75	5
	CVLL		592		8.5
	CVC		145		3,5
2	CV	98	245	M12x1.75	5
-	CVL	00	419		7
	CVC		150		3.5
	CV	00	250	M10x1 75	5
3	CVL	90	439	W12X1,75	7,5
	CVLL		643		9,5
	CVC CV		250		5
4	CVL	98	442	M12x1,75	7,5
	CVLL		649		9
	CVC		155		4
5	CVL	98	455	M12x1,75	7.5
	CVLL		667		9
	CVC		165		7
6	CV	134	265	M12x1,75	9
	CVL		693		14
	CVC		170		7
7	CV	134	275	M16x2	10
i i	CVL		505		15
	CVLL		180		7.5
	CV	104	295	1440-0	11
8	CVL	134	540	MITOX2	17
	CVLL		785		20
			305		8
9	CVL	134	565	M16x2	18
	CVLL		825		22
	CVC		195		8
10		134	580	M20x2,5	12
	CVLL		845		24
	CVC		220		18
11	CV	168	345	M20x2,5	23
			625 905		35
	CVC		230		19
12	CV	168	360	M24v3	25
12	CVL	100	655	WZ4X3	38
			950		47
10	CV CV	100	375	140.4 0	27
13	CVL	168	680	M24x3	43
	CVLL		985		50
			255		23
14	CVL	168	750	M30x3,5	50
	CVLL		1090		55
	CVC		265		46
15	CVI	236	735	M30x3,5	89
	CVLL		1065		114
	CVC		280		52
16	CV	236	435 70F	M36x4	67
	CVL		1155		138
	CVC		305		59
17	CV	236	480	M36x4	79
	CVL		890		130
	CVC		325		106
18	CV	304	485	M42x4 5	134
	CVL	504	870	101 TZAT,0	204
			1250		1202
40	CV	004	530	M40 5	152
19	CVL	304	960	M48x5	243
	CVLL		1385		323
			370		138
20	CVL	304	1010	M56x5,5	291
	CVLL		1455		390
	CVC		395		160
21		304	655	M64x6	219
	CVLL		1765		520

3	21/07/10	GENERAL REVISION	DDG	EAR
2	12/07/91	INFORMATION	JMD	EAR
1	17/01/85	INFORMATION	JRS	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



VARIABLE LOAD SPRING SUPPORT TYPE F

SECTION D 19



<u>N.B.:</u>

For this type of spring, a PTFE plate or bronze-graphite plate can optionally be installed on the load plate.

PTFE	BRONZE - GRAPHITE

				21
3	21/07/10	GENERAL REVISION	DDG	EAR
2	12/07/91	INFORMATION	JMD	EAR
1	17/01/85	INFORMATION	JRS	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.

0175	MOD	S S					ат	WEIGHT	
SIZE	MOD.	MIN.	MAX.	ØA	ЮН	ωŪ	٧W	וש	(Kg.)
	CVC	192	242						5
1	CV	287	337	98	17.5	155	195	95	6,5
1		452	502		,•				9
	CVLL	192	242						5
2	CV	292	342	00	175	155	105	05	6,5
2	CVL	466	516	90	17,5	155	195	95	9
		686	736						11
		297	347						ວ 65
3	CVL	486	536	98	17,5	155	195	95	9,5
	CVLL	716	766						12
	CVC	197	247						6
4		297	547 540	98	17,5	155	195	95	95
	CVLL	722	772						12
	CVC	202	252						6
5	CV	307	357	98	17,5	155	195	95	7
		502 740	552 790						9,5
	CVLL	227	277						9
6	CV	327	377	13/	17.5	100	230	120	11
0	CVL	539	589	134	11,0	130	230	120	16
		232	820 282						20
7	CV	337	387	40.4	175	100	000	100	12
'	CVL	567	617	134	17,5	190	230	120	17
	CVLL	813	863	_					21
		242	292						10
8	CVL	602	652	134	17,5	190	230	120	19
	CVLL	863	913						23
	CVC	252	302						10
9		367	41/	134	17,5	190	230	120	13
		903	953						20
	CVC	257	307						11
10	CV	377	427	134	17.5	190	230	120	15
		642	692		,•		200	0	21
	CVLL	<u>923</u> 291	973 341						20
44	CV	416	466	100	21 5	225	205	150	28
11	CVL	695	745	168	21,5	225	265	150	40
	CVLL	990	1040						49
		431	301 481						23
12	CVL	725	775	168	21,5	225	265	150	44
	CVLL	1035	1085						53
		306	356						25
13		750	496 800	168	21,5	5 225	265	150	32 47
	CVLL	1070	1120						56
	CVC	326	376						26
14	CV	481	531	168	21,5	225	265	150	34
		820	870						54 64
	CVC	363	413						55
15	CV	503	553	236	21.5	295	335	220	68
10		835	885	200	2.,0	200	000	220	98
	CVLL	378	428						59
40	CV	533	583	000	01 5	005	0.05	000	76
16	CVL	895	945	236	21,5	295	335	220	114
	CVLL	1250	1300						144
		403 578	453						86
17	CVL	990	1040	236	21,5	295	335	220	134
	CVLL	1385	1435						174
	CVC	433	483						114
18		980	043 1030	304	21,5	365	405	275	208
	CVLL	1355	1405						266
	CVC	463	513						125
19	CV	638	688	304	21,5	365	405	275	157
-		10/0	1120		,				250
	CVC	478	528						145
20	CV	663	713	304	215	365	405	275	173
20	CVL	1120	1170	504	21,0	303	-00	215	300
		1550	1600						410
04	CV CV	795	845	204	21 5	205	405	075	215
21	CVL	1355	1405	304	21,5	365	405	2/5	387
	CVLL	1915	1965						537

solutions

pipe hanger

VARIABLE LOAD SPRING SUPPORT TYPE G



SIZE	MOD.	в	С	Y	ØA	ØR	Х	2 UPN	W (MAX.)
	CVC	145	45	20					
4	CV	240	10	30	00	M12v1 75	20	00	2500
1	CVL	405	10	50	90	11/12x1,75	20	00	2500
	CVLL	592	10	70					
	CVC	145	45	20					
2	CV	245	10	30	98	M12x1.75	20	80	2500
-	CVL	419	10	50					
		150	10	70					
		250	45	20					
3	CVI	439	10	50	98	M12x1,75	20	80	2500
	CVLL	643	10	70					
	CVC	150	45	20					
Δ	CV	250	10	30	98	M12x1 75	20	80	2500
	CVL	442	10	50	00		20	00	2000
	CVLL	649 155	10	70					
		255	40	20					
5	CVL	455	10	50	98	M12x1,75	20	80	2500
	CVLL	667	10	70					
	CVC	165	50	20					
6	CV	265	15	30	134	M12x1.75	28	100	2500
, i i i i i i i i i i i i i i i i i i i	CVL	477	15	50					
	CVLL	170	15	70					
	CVC	275	15	30					
7	CVL	505	15	50	134	M16x2	28	100	2500
	CVLL	735	15	70					
	CVC	180	50	20					
8	CV	295	15	30	134	M16x2	28	100	2500
•	CVL	540	15	50					
		100	15	70					
		305	25	30					
9	CVL	565	25	50	134	M16x2	28	100	2500
	CVLL	825	25	70					
	CVC	195	55	20					
10	CV	315	25	30	134	M20x2.5	28	100	2500
	CVL	580	25	50		,.	_0		2000
		845 220	20 55	70					
	CV CV	345	25	40					
11	CVL	625	25	60	168	M20x2,5	36	140	2500
	CVLL	905	25	80					
	CVC	230	55	20					
12	CV	360	25	40	168	M24x3	36	140	2500
		655 050	25	60 80					
	CVC	235	50	20					
40	CV	375	25	40	100		~~		0500
13	CVL	680	25	60	168	M24x3	36	140	2500
	CVLL	985	25	80					
	CVC	255	70	20					
14		410	30	40	168	M30x3,5	36	140	2500
		1090	30	80					
	CVC	265	80	20					
15	CV	405	30	40	226	M30v3 5	50	220	2500
15	CVL	735	30	60	230	1013073,3	50	220	2500
	CVLL	1065	30	80					
		280	80	20					
16	CVI	795	40	40 60	236	M36x4	50	220	2500
	CVLL	1155	40	80					
	CVC	305	80	20					
17	CV	480	40	40	236	M36v4	50	220	2500
17	CVL	890	40	60	200	1013024	50	220	2000
	CVLL	1290	40	80					
		323 485	40	50			_	220	1400
18	CVL	870	40	80	304	M42x4,5	66	000	0500
	CVLL	1250	40	110				300	2500
	CVC	355	60	15				220	1400
19	CV	530	40	50	304	M48x5	66		
		960	40	80				300	2500
	CVC	370	40 60	15					
00	CV CV	555	40	50	004	MEQUE	00	220	1400
20	CVL	1010	40	80	304	1112025,5	66	200	2500
	CVLL	1455	40	110				300	2500

<u>N.B.:</u>

The weight of the unit will be double the corresponding "E" type spring, plus the weight of the sections with length= W-A.

* C is an approximate dimension which corresponds to the vertical position at the lowest load value of the working range. Therefore, the actual dimension will vary depending on the load applied.

3	21/07/10	GENERAL REVISION	DDG	EAR
2	12/07/91	INFORMATION	JMD	EAR
1	17/01/85	INFORMATION	JRS	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



VARIABLE LOAD SPRING SUPPORT TYPE H

SECTION D





1	21/07/10	GENERAL REVISION	DDG	EAR
0	20/10/98	INFORMATION	JMD	EAR
REV	DATE	EDITED FOR :	DRAW.	REV.

TUBE



SPECIAL CORROSION RESISTANT VARIABLE SPRINGS WITH CONTINUOUS BLOCKING SYSTEM

The standard surface finish is a two-coat epoxy-polyure thane paint system, with a total dry film thickness of approximately 100 $\mu m.$

However, when environmental conditions are particularly severe, we are ready to apply special surface treatments that further protect the spring support against corrosion, either by the application of more complex paint systems (three or even four coats up to 200-300 μ m DFT) or by hot dip galvanizing the spring casing, once specified and agreed with the client.

Special corrosion resistant variable springs with hot dip galvanized casing use a hybrid welded/bolted construction, while standard variable springs are all welded.

In addition, special corrosion resistant variable springs with hot dip galvanized casing include the continuous blocking system, so the spring can be blocked at any working position, while standard variable springs use travel stops that are also valid for blocking at the unique cold preset load that is specified for each individual unit.

The continuous blocking system can also be used to establish a limited travel range or specific load stops.

Selection of spring model, size and type for special corrosion resistant supports with continuous blocking system is the same as with standard supports.

DESCRIPTION OF THE CONTINUOUS BLOCKING SYSTEM

The purpose of the continuous blocking system in the variable load spring supports manufactured at PIHASA is the capacity to block the spring in any working position, with the following requirements:

- Block the support by absorbing the expansion strength of the spring itself, in each position.
- At the same time, the purpose is to block the spring in terms of compression (downwards), being able to support loads during the inspection and assembly stage. The value achieved in these stages is up to two and a half times the operating load.
- Blocking should act on all the travel range of the spring.
- The system will continue to be available in the support housing throughout the life cycle of the spring, so that it allows for blocking whenever required.

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.





VARIABLE LOAD SPRINGS WITH CONTINUOUS BLOCKING SYSTEM

1.- BLOCKING PROCESS:

- 1.1 Having completed the surface finish operations (PIHASA standards or any specified by the client), proceed to blocking the support. The rods and nuts are electro-galvanized to ensure protection against corrosion.
- 1.2 Once the spring has been calibrated to its cold preset load/position, tighten up the lower and upper nuts on the guides against the load plate.
- 1.3 The upper side of the load plate should coincide with the installation load mark or cold mark of the scaleplate.

2.- INSTALLATION INSTRUCTIONS - UNBLOCKING THE SYSTEM:

Please first read sheets D7-D13 for a description of the different types. The blocking system does not affect the way of installing the support, but only affects the way of blocking and unblocking it.

The upper and lower blocking nuts should be in permanent contact with the load plate until such time as it is decided to proceed with the unblocking manoeuvres, which should be carried out once known that no loads other than operational loads are going to occur, such as in the hydraulic test, during cleaning operations or in the course of other situations.

The unblocking process involves following these steps:

• First, loosen the lower blocking nuts and turn them (on both sides) till they reach the end of the spring travel, as indicated on the support scaleplate.

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



- Then, tighten up the support to reach the installation or cold load (weight of the piping at the point where the support is installed). This operation involves:
 - Acting on the adjusting turnbuckles (types A-B-C-E or G).
 - Acting on the upper nuts on the hanging rod on supports installed on the structure (Type D).
 - Acting on the threaded load column on supports installed on the ground (Type F).
- The installation load is reached when the load plate starts to move downwards.
- The final step is to loosen the upper blocking nuts until reaching the start of the spring travel: point "O" indicated on the label.

SUPPLEMENTARY NOTES:

- For any subsequent operation on the piping system, it is essential to first block the support in order to prevent modifications in the work conditions of the support. This is achieved by tightening the upper and lower blocking nuts until they come into contact with the load plate. Then, unblock by following the steps in point 2 of these instructions.
- The continuous blocking system on PIHASA's variable load supports makes it possible to insert travel limits. These limits can be set to avoid the spring going past certain points (upwards or downwards) if this is required by the engineering company. Quite simply, this is achieved by setting the upper and/or lower blocking nuts in the required position.

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.



CORROSION RESISTANT VARIABLE LOAD SECTION D SUPPORTS WITH CONTINUOUS BLOCKING SYSTEM

26



0	21/07/10	GENERAL REVISION	DDG	EAR	
REV.	DATE	EDITED FOR :	DRAW.	REV.	



OPERATION AND MAINTENANCE OF SPRING SUPPORTS

OPERATION AND MAINTENANCE RECOMMENDATIONS FOR SPRING SUPPORTS:

In the course of the normal operation of elastic supports (variable load or constant load spring supports), there is no need for a direct action on the same during service or operation in the plant. But on the other hand, preventive maintenance tasks are recommended to be performed on a regular basis. These involve a regular visual inspection (this can often be done using binoculars) to evaluate the general status of cleanness, rust, as well as to detect any potential important anomalies such as deformed components, the presence of external interferences limiting movement, loose and unthreaded parts, etc.

In the event of detecting anomalies in the course of the visual inspection, or as a recommended practice once every 5-10 years, and more frequently in corrosive conditions more prone to rusting or environmental fouling, or in the case of significant vibrations, or pressure shocks, we suggest acting physically on each spring support during plant shutdowns ("cold inspection"), performing the following activities:

- Cleaning, removing grease and fouling.
- Retouch painting.
- Greasing threaded parts.
- Replacing scaleplates (if lost or deteriorated).
- Check tags and markings.
- Check the position of the load indicator and compare with the theoretical position (cold or installation position) and adjust using the spring adjustment elements to reach the theoretical position if appropriate (evaluated by the technical department).
- Any other incident, such as: interferences, degrees of rust, etc.

After these inspections, it is advisable to draft historical reports. In the course of visual inspections or direct checks, when noting a notable deterioration or highly significant or recurrent deviations from the work positions on the load indicator, consideration should be given to replacing the support with a new one or, alternatively, carry out a more thorough revision of the supports.

Revisions are more complete inspections, with the following characteristics:

- * Carried out by specialised companies during the programmed maintenance stops.
- * In addition to the regular periodic inspection activities, the following operations are performed:
- Disassemble variable or constant load supports in order to proceed to internal and external cleaning.
- Full calibration of variable and constant spring supports obtaining load-displacement functional graphs.
- These graphs show the "k" spring rate for the variable supports and the variability of load in the constants, apart from the operating load deviation for both supports.
- All the information compiled is included in a final revision Dossier, where all the comments and recommendations that the company specializing in inspections considers essential are noted, based on objective data (relevant regulations) and acceptance criteria arising from the experience itself.

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.









ORDER FORM:

- Name.

- Figure.
- Pipe diameter.

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.





<u>APPLICATION</u>: As an element for mitigating vibrations in pipelines. The load level, adjusted by tightening nuts on the spring, should be set by the engineering company, within the specified range.

ORDER FORM:

- Name.
- Figure.
- Pipe diameter.

0	21/07/10	GENERAL REVISION	DDG	EAR
REV.	DATE	EDITED FOR :	DRAW.	REV.

